

Čestični metodi za simulacije kompleksnih sistema

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Različiti pristupi u modelovanju

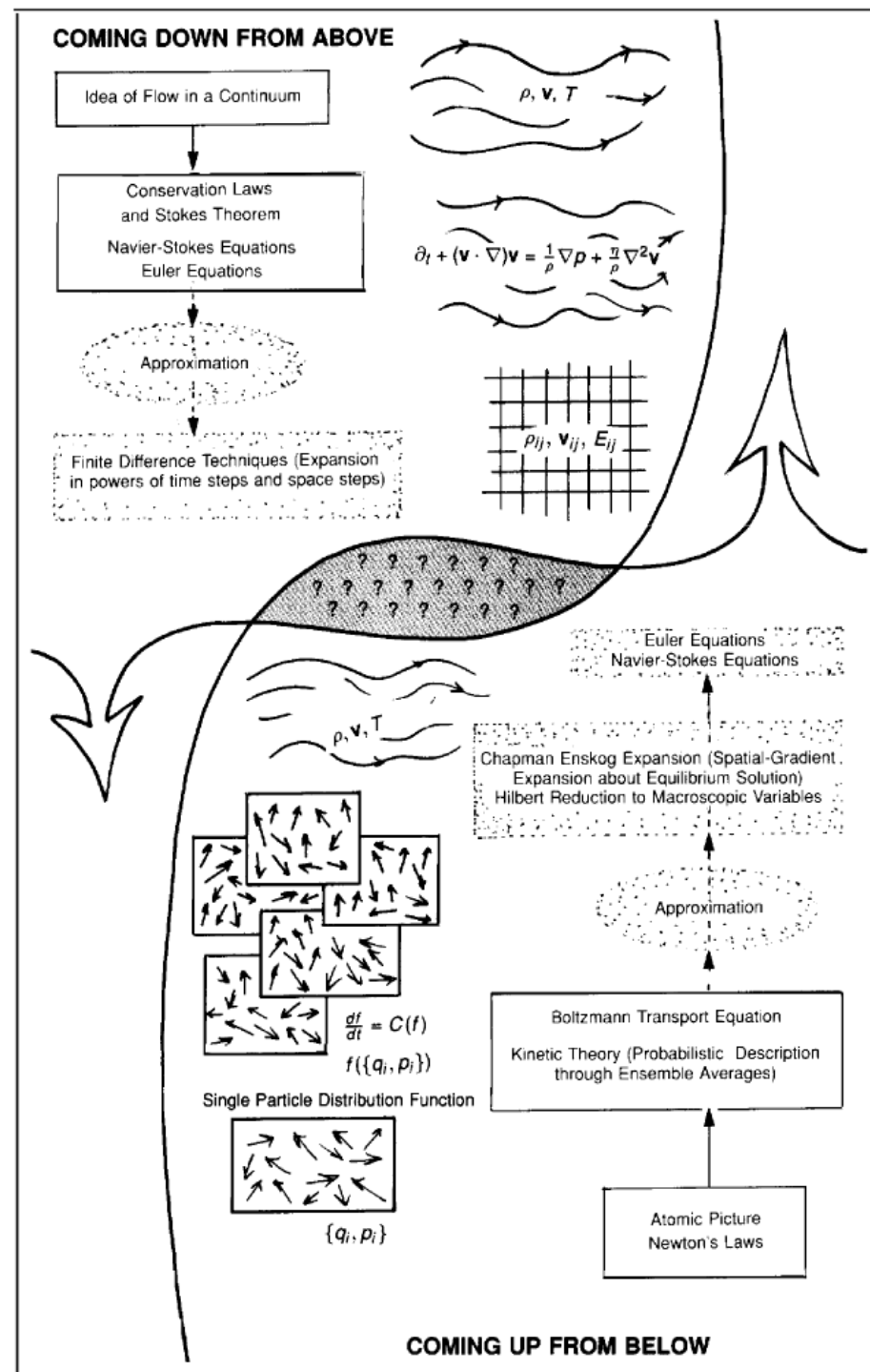


Fig. 2. Both the continuum view of fluids and the atomic picture lead to the Navier-Stokes equations but not without approxima-

tions (dashed lines). The text emphasizes how cellular-automaton models embody the essentials of both points of view.

Mehanika fluida - ukratko

Posmatrani element Σ mora biti dovoljno

- (1) veliki da molekularna strukutra može da se zameni kontinualnim modelima
- (2) dovoljno mali da bi bio matematički prihvatljiv

onda geometrijskih razmatranja + $\oint_{\partial\Sigma} \mathbf{A} \cdot d\mathbf{l} = \oint_{\Sigma} \nabla \times \mathbf{A} \cdot d\mathbf{S}$ & $\oint_{\partial\Sigma} \mathbf{A} \cdot d\mathbf{S} = \int_{\Sigma} \nabla \cdot \mathbf{A} dV$
 dobija se:

$$\overbrace{\oint_{\partial\Sigma} \rho \mathbf{v} \cdot d\mathbf{S}}^{\text{flux of mass}} = -\partial_t \overbrace{\int_{\Sigma} \rho dV}^{\text{mass}} = \int_{\Sigma} \nabla \cdot (\rho \mathbf{v}) dV \xrightarrow{\Sigma \rightarrow 0} \boxed{\partial_t \rho + \nabla \cdot (\rho \mathbf{v}) = 0} \begin{array}{l} \text{jednačina} \\ \text{kontinuiteta} \end{array}$$

pritisak je sila na jedinicu zapremine

$$-\oint_{\partial\Sigma} p d\mathbf{S} = -\int_{\Sigma} \nabla p dV \quad \mathbf{F} = m \mathbf{a} = \int_{\Sigma} \rho \frac{d\mathbf{v}}{dt} dV \xrightarrow{\Sigma \rightarrow 0} -\nabla p = \rho \frac{d\mathbf{v}}{dt} \rightarrow \boxed{\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla) \mathbf{v} = -\frac{1}{\rho} \nabla p} \begin{array}{l} \text{Eulerova} \\ \text{jednačina} \end{array}$$

$$\boxed{\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla) \mathbf{v} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{v}} \begin{array}{l} \text{Navier-Stoksova} \\ \text{jednačina} \end{array}$$

Mehanika fluida - ukratko

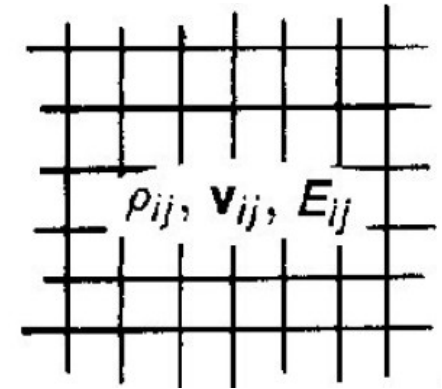
$$\partial_t \rho + \nabla \cdot (\rho \mathbf{v}) = 0$$

$$\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla) \mathbf{v} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{v}$$

$$(\partial_t f)_{ij}^n \approx \frac{f_{ij}^{n+1} - f_{ij}^n}{\Delta t}$$

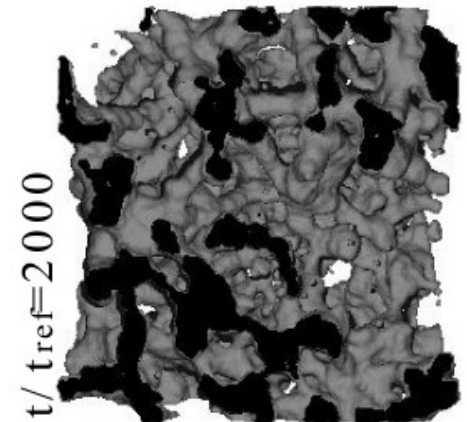
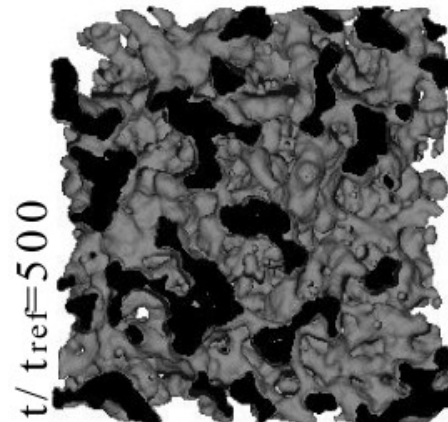
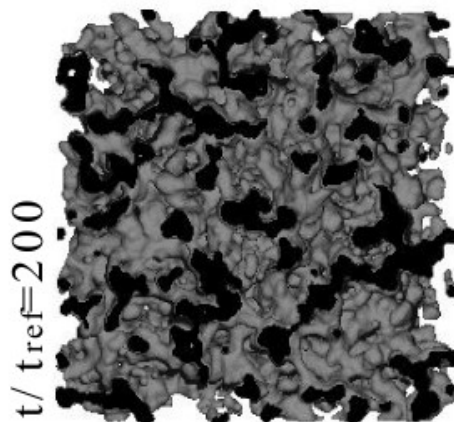
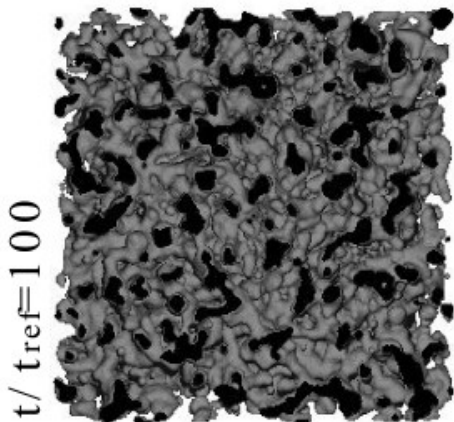
$$(\nabla_x f)_{ij}^n \approx \frac{f_{i+1,j}^n - f_{i,j}^n}{\Delta x}$$

$$(\nabla_x^2 f)_{ij}^n \approx \frac{f_{i+1,j}^n - 2f_{i,j}^n + f_{i,j-1}^n}{2\Delta x^2}$$



rešite diskretizovane
numeričke jednačine na
mreži tačaka

Šta ne može da reši mehanika fluida

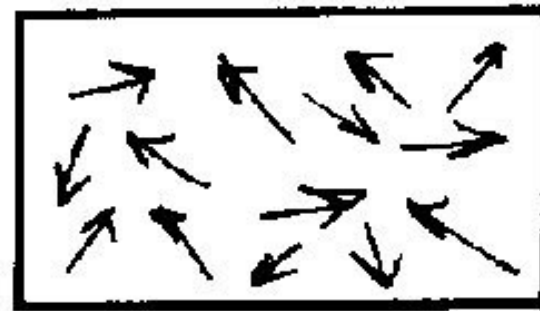


Pristup na malim skalama - ukratko

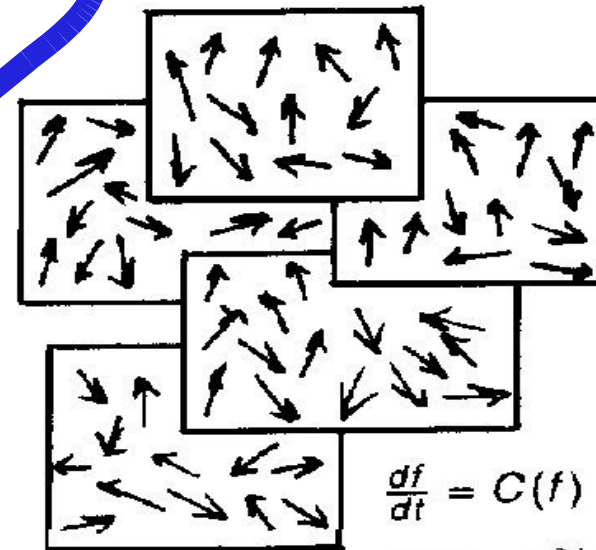
Čestice, atomi ili molekuli interaguju preko klasičnih (ili kvantnih) potencijala

$$\dot{\mathbf{r}}_i = \mathbf{v}_i$$

$$\dot{\mathbf{v}}_i = -\nabla_i U(\mathbf{r}_1, \dots, \mathbf{r}_N)$$



$$\{q_i, p_i\}$$



$$\frac{df}{dt} = C(f)$$

$$f(\{q_i, p_i\})$$

Single Particle Distribution Function

$$\langle n(\mathbf{r}, t) \rangle = \int f(t, \mathbf{r}, \mathbf{v}) d\mathbf{v}$$

$$\langle \mathbf{V}(\mathbf{r}, t) \rangle = \frac{1}{\langle n \rangle} \int f(t, \mathbf{r}, \mathbf{v}) \mathbf{v} d\mathbf{v}$$

srednje vrednosti iz jednočestične funkcije raspodele

Postoji li direktan prelaz iz kontinualnih u čestične modele

molekularni:

- neravnotežna molekularna dinamika (NEMD)
- Monte Karlo (MC)

mezoskopski metodi:

- Boltzmanovu jednačinu na rešetci (LB)
- braunovska dinamika (BD),
- disipativna čestična dinamika (DPD)

makroskopski metodi:

- hidrodinamika ujednačenih čestica (SPH)

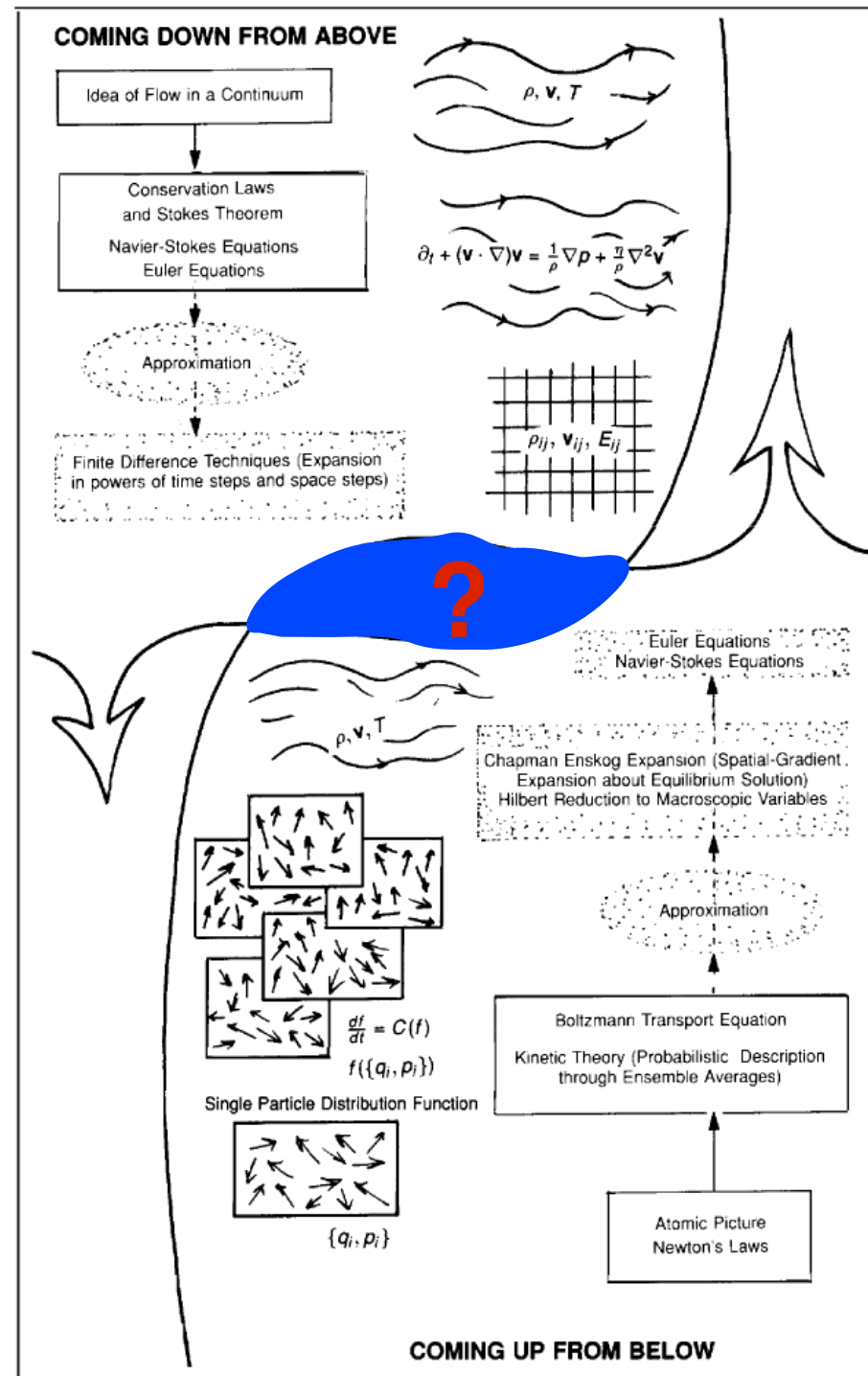


Fig. 2. Both the continuum view of fluids and the atomic picture lead to the Navier-Stokes equations but not without approxima-

tions (dashed lines). The text emphasizes how cellular-automaton models embody the essentials of both points of view.

Metod molekularne dinamike

$$\begin{aligned}\dot{\mathbf{r}}_i &= \mathbf{v}_i \\ \dot{\mathbf{v}}_i &= -\nabla_i V(\mathbf{r}_1, \dots, \mathbf{r}_N)\end{aligned}$$

molekuli, atomi

$$V(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N) = \sum_i \sum_{j>i} \phi(|\mathbf{r}_i - \mathbf{r}_j|)$$

$$\phi_{LJ}(r) = 4\epsilon \left[\left(\frac{\sigma}{r} \right)^{12} - \left(\frac{\sigma}{r} \right)^6 \right]$$

metali, poluprovodnici

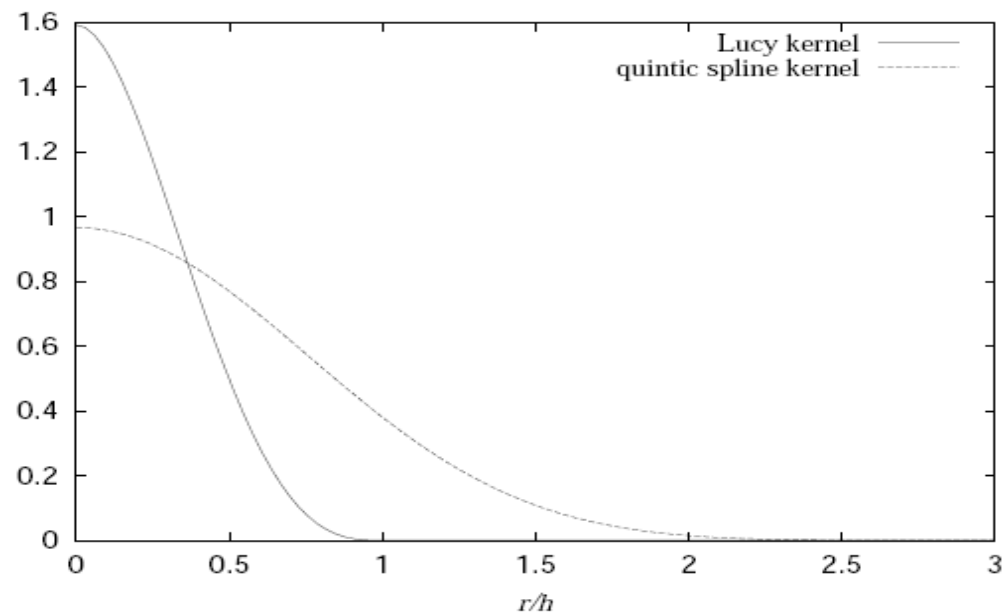
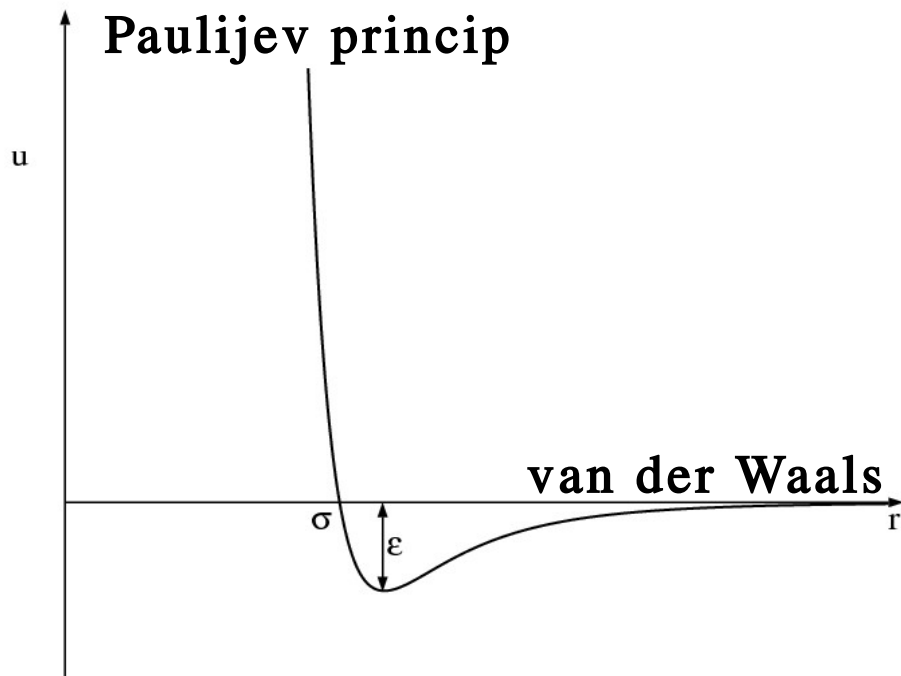
$$V(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N) = \sum_i \left(\sum_{j>i} \phi(|\mathbf{r}_i - \mathbf{r}_j|) + \Theta(\rho_i) \right)$$

$$\Theta(\rho_i) = \phi_0 \sum_{k=2,4,\dots} r_0^3 k F_k ((\rho_i - \rho_{des})^k - (w(0) - \rho_{des})^k)$$

lokalna gustina

$$\rho_i = \sum_j w(r_{ij})$$

$$w(r) = w_0 \left(1 + 3 \frac{r}{r_{cut}} \right) \left(1 - \frac{r}{r_{cut}} \right)^3$$



Metod molekularne dinamike

$$V(t) = \sum_i \sum_{j>i} \phi(|\mathbf{r}_i(t) - \mathbf{r}_j(t)|) \quad \text{potencijalna energija}$$

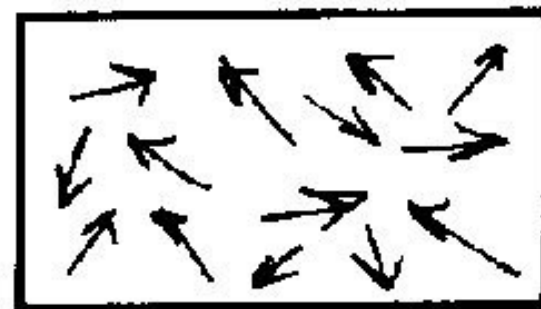
$$K(t) = \frac{1}{2} \sum_i m_i [v_i(t)]^2 \quad \text{kinetička energija}$$

$$E(t) = K(t) + V(t)$$

$$K(t) = \frac{3}{2} N k_B T(t) \quad \text{temperatura}$$

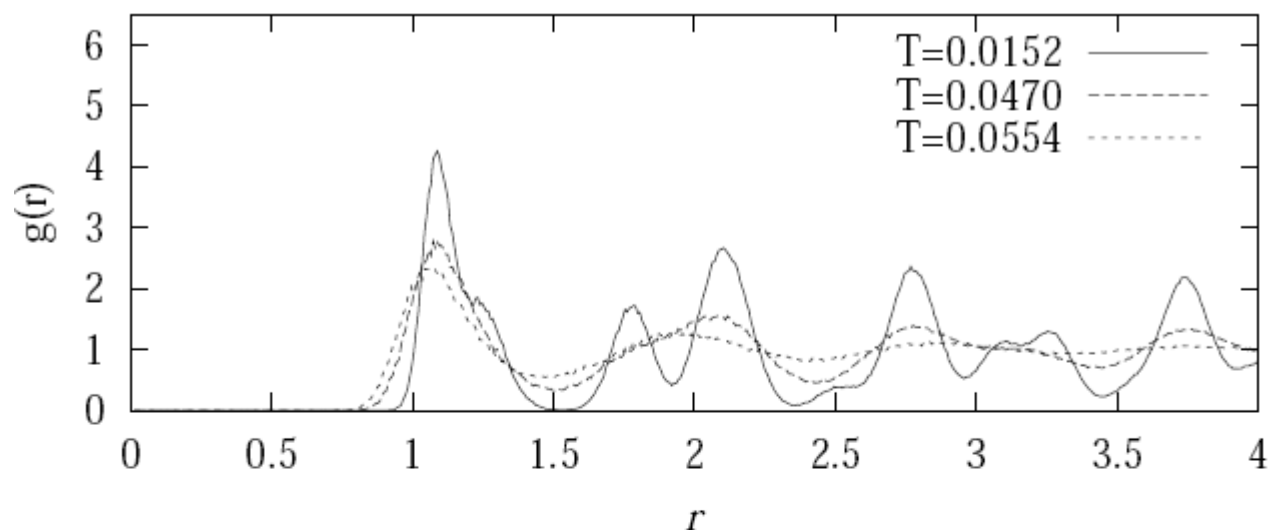
$$PV = N k_B T - \frac{1}{3} \left\langle \sum_i \mathbf{r}_i \cdot \mathbf{F}_i \right\rangle \quad \text{pritisak}$$

$$D = \lim_{t \rightarrow \infty} \frac{1}{6t} \langle |\mathbf{r}(t) - \mathbf{r}(0)|^2 \rangle \quad \text{koeficijent difuzije}$$

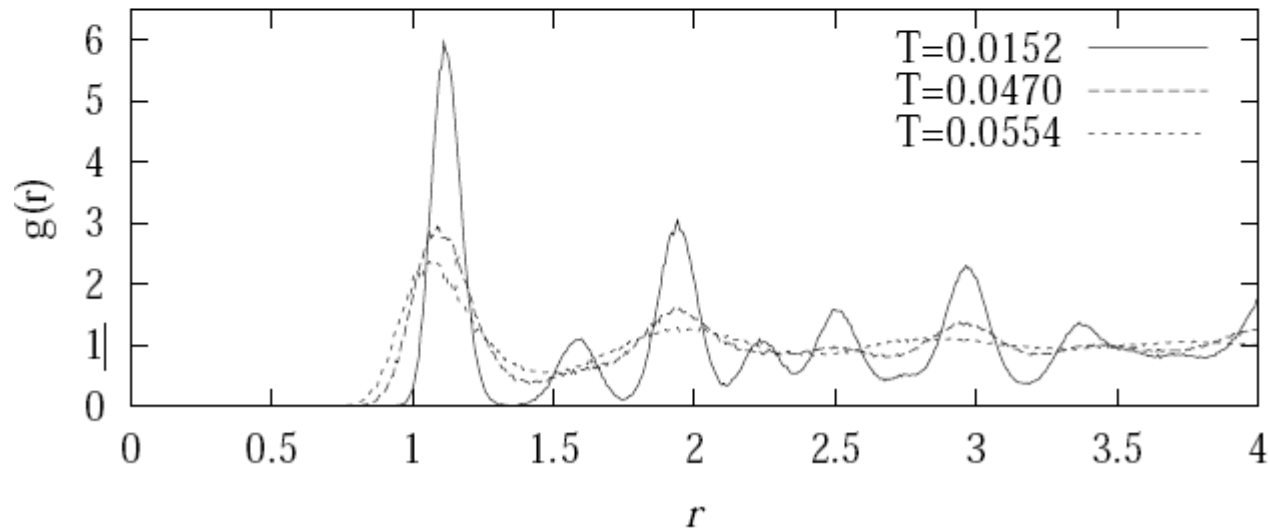


$\{q_i, p_i\}$

Metod molekularne dinamike



a) body-centered cubic structure



b) face-centered cubic structure

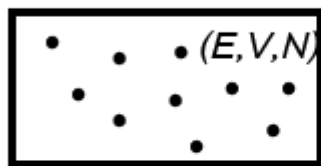
$$\rho g(r) = \frac{1}{N} \left\langle \sum_i \sum_{j \neq i} \delta(r - r_{ij}) \right\rangle$$

dvočestična funkcija
raspodele

Metod molekularne dinamike

- Microcanonical ensemble

isolated system

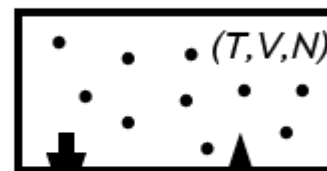


*energy transfer not
allowed
E constant*

$$f(\Gamma) = \delta(H(\Gamma) - E)$$

- Canonical ensemble

heat reservoir T



*energy transfer
allowed
T constant*

$$f(\Gamma) = \exp(-H(\Gamma)/k_B T)$$



potrebne su dodatne
jednačine

Metod molekularne dinamike

Nose-Hoover termostat

$$\dot{\mathbf{r}}_i = \frac{\mathbf{p}_i}{m_i}$$

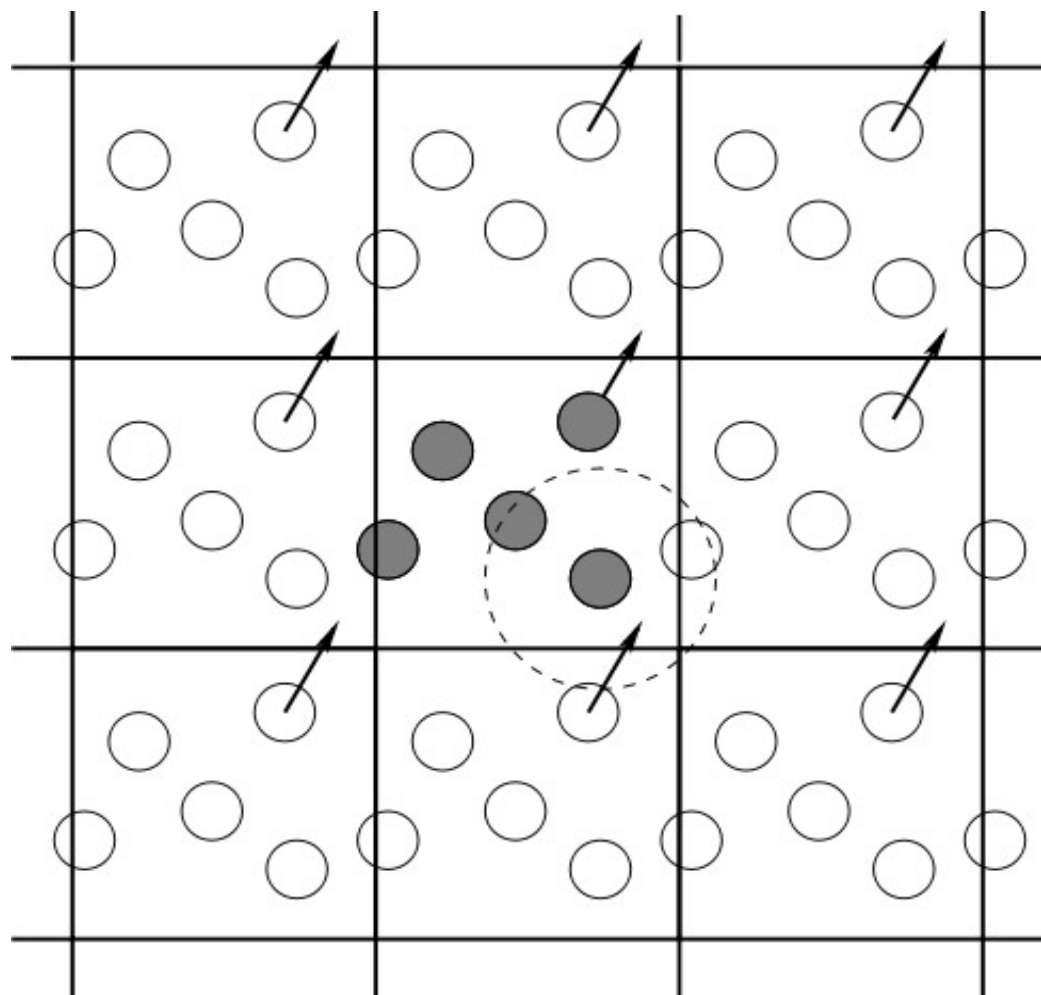
$$\dot{\mathbf{p}}_i = -\nabla_i V - \zeta \mathbf{p}_i$$

$$\dot{\zeta} = \frac{\left(\sum_i \frac{\mathbf{p}_i^2}{m_i} - g k_B T \right)}{Q} = \nu_\tau \left[\frac{\sum_i \frac{\mathbf{p}_i^2}{m_i}}{g k_B T} - 1 \right] = \nu_\tau \left[\frac{T^*}{T} - 1 \right]$$

Woodcock termostat

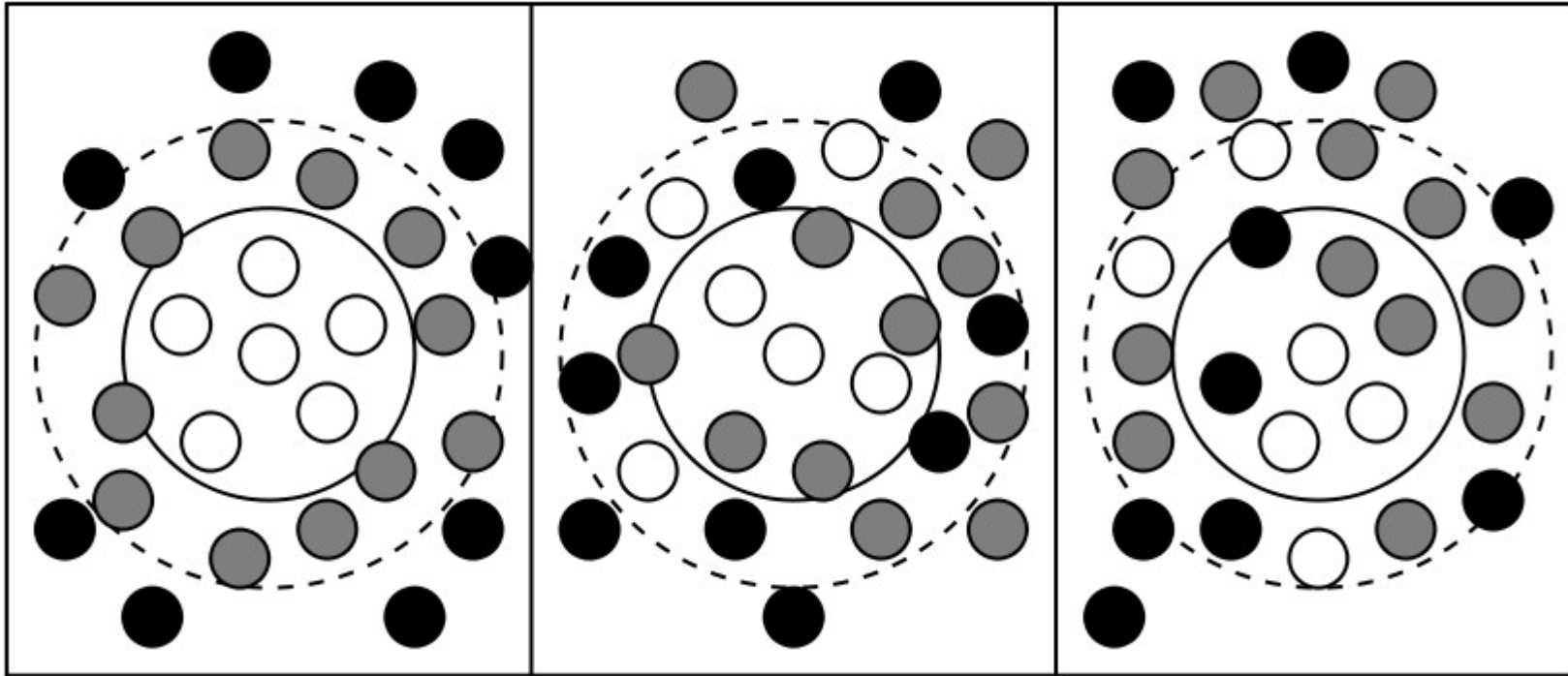
$$\hat{\mathbf{v}}_i \left(t + \frac{\Delta t}{2} \right) = S \mathbf{v}_i \left(t + \frac{\Delta t}{2} \right) \quad \longrightarrow \quad S = \left[\frac{\frac{3}{2} N k_B T}{\sum_i \frac{m_i}{2} \left[\mathbf{v}_i \left(t + \frac{\Delta t}{2} \right) \right]^2} \right]^{1/2}$$

Metod molekularne dinamike



periodični granični uslovi

Metod molekularne dinamike



liste suseda za smanjivanje kompleksnosti problema

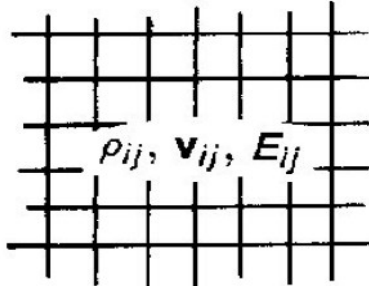
Mehanika fluida - ukratko

$$\begin{aligned} \partial_t \rho + \nabla \cdot (\rho \mathbf{v}) &= 0 \\ \partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla) \mathbf{v} &= -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{v} \end{aligned}$$

→

$$\begin{aligned} (\partial_t f)_{ij}^n &\approx \frac{f_{i,j}^{n+1} - f_{i,j}^n}{\Delta t} \\ (\nabla_x f)_{ij}^n &\approx \frac{f_{i+1,j}^n - f_{i-1,j}^n}{\Delta x} \\ (\nabla_x^2 f)_{ij}^n &\approx \frac{f_{i+1,j}^n - 2f_{i,j}^n + f_{i-1,j}^n}{2\Delta x^2} \end{aligned}$$

→



Hidrodinamika ujednačenih čestica (SPH)

$$\langle f(\mathbf{x}) \rangle = \int_{\Omega} f(\mathbf{x}') W(\mathbf{x} - \mathbf{x}', h) d\mathbf{x}'$$

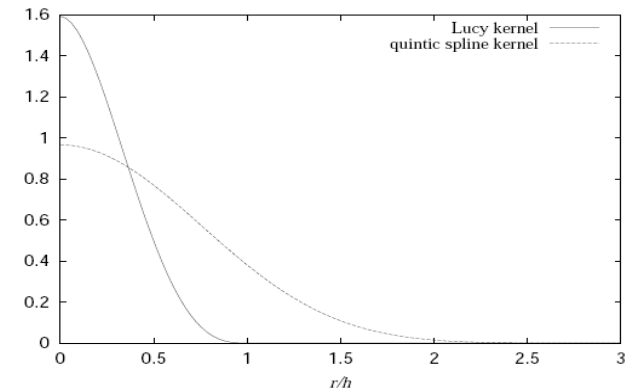
$$\int_{\Omega} W(\mathbf{x} - \mathbf{x}', h) d\mathbf{x}' = 1,$$

$$\lim_{h \rightarrow 0} W(\mathbf{x} - \mathbf{x}', h) = \delta(\mathbf{x} - \mathbf{x}')$$

$$n(\mathbf{x}) = \sum_j \delta(\mathbf{x} - \mathbf{x}_j)$$

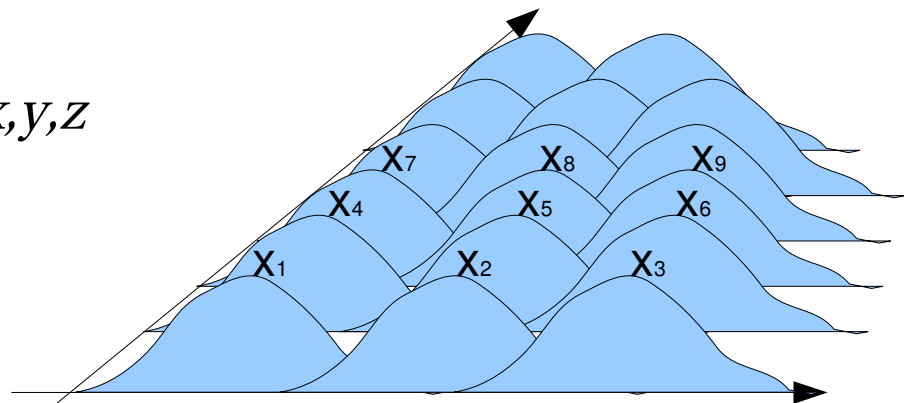
dx je zamenjen
zapreminom čestice

$$d\mathbf{x}' \rightarrow \phi_j \equiv \frac{m_j}{\rho_j}$$



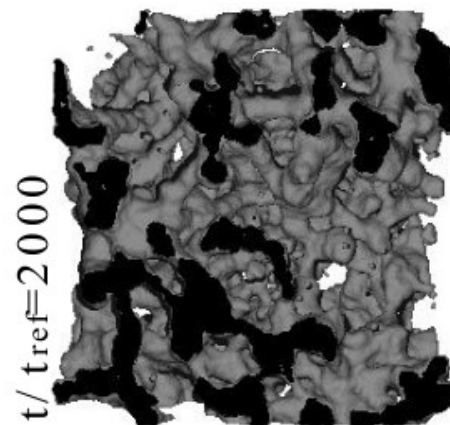
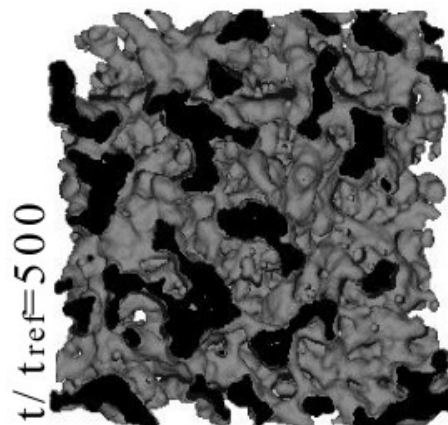
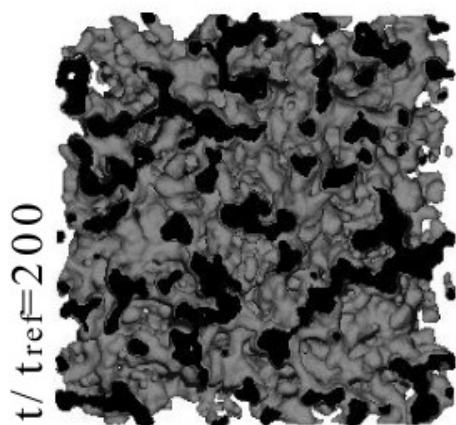
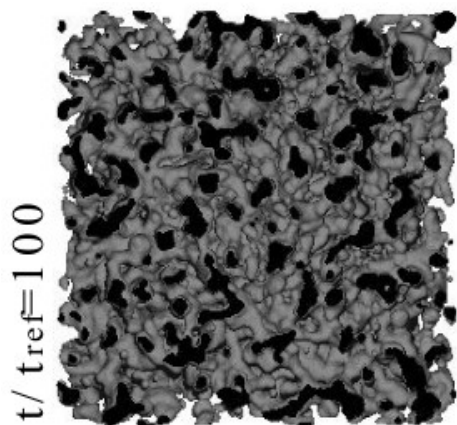
Hidrodinamika ujednačenih čestica (SPH)

$$\frac{\partial V^\alpha}{\partial t} + (V^\beta \nabla^\beta) V^\alpha = \frac{1}{\rho} \nabla^\beta P^{\alpha\beta}, \quad \alpha, \beta = x, y, z$$



$$\int_{\Omega} \left(\frac{\partial V^\alpha}{\partial t} + (V^\beta \nabla'^\beta) V^\alpha \right) W(|\mathbf{x} - \mathbf{x}'|, h) d\mathbf{x}' = \int_{\Omega} \left(\frac{1}{\rho} \nabla'^\beta P^{\alpha\beta} \right) W(|\mathbf{x} - \mathbf{x}'|, h) d\mathbf{x}'$$

$$\frac{dV_i^\alpha}{dt} = \sum_j m_j \left(\frac{P_i^{\alpha\beta}}{\rho_i^2} + \frac{P_j^{\alpha\beta}}{\rho_j^2} \right) \nabla_i^\alpha W_{ij}$$

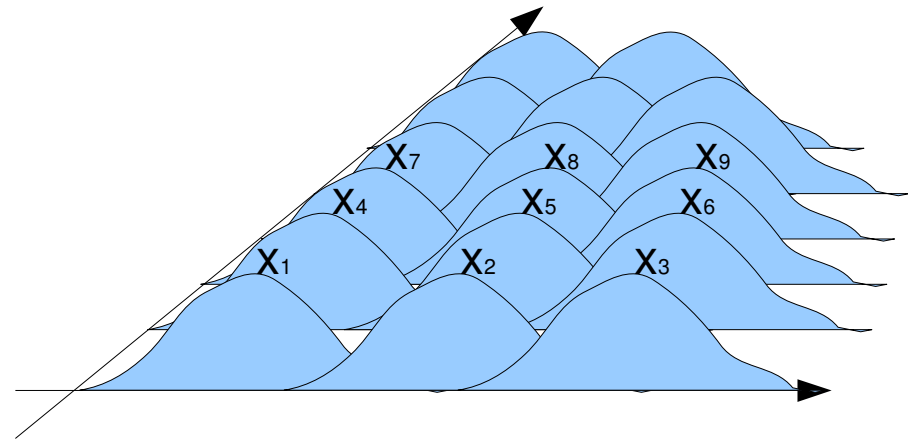


Hidrodinamika ujednačenih čestica (SPH)

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$P \sim \rho^2$

$$\begin{aligned} \dot{\mathbf{r}}_i &= \mathbf{v}_i \\ \dot{\mathbf{v}}_i &= -\nabla_i V(\mathbf{r}_1, \dots, \mathbf{r}_N) \end{aligned}$$



Kako integrirati dve skale?

$$\frac{dV_i^\alpha}{dt} = \sum_j m_j \left(\frac{P_i^{\alpha\beta}}{\rho_i^2} + \frac{P_j^{\alpha\beta}}{\rho_j^2} \right) \nabla_i^\alpha W_{ij}$$

interpretacija
čestice



pritisak

površinski napon

termostat

$$\dot{\mathbf{r}}_i = \mathbf{v}_i$$

$$\dot{\mathbf{v}}_i = -\nabla_i V(\mathbf{r}_1, \dots, \mathbf{r}_N)$$

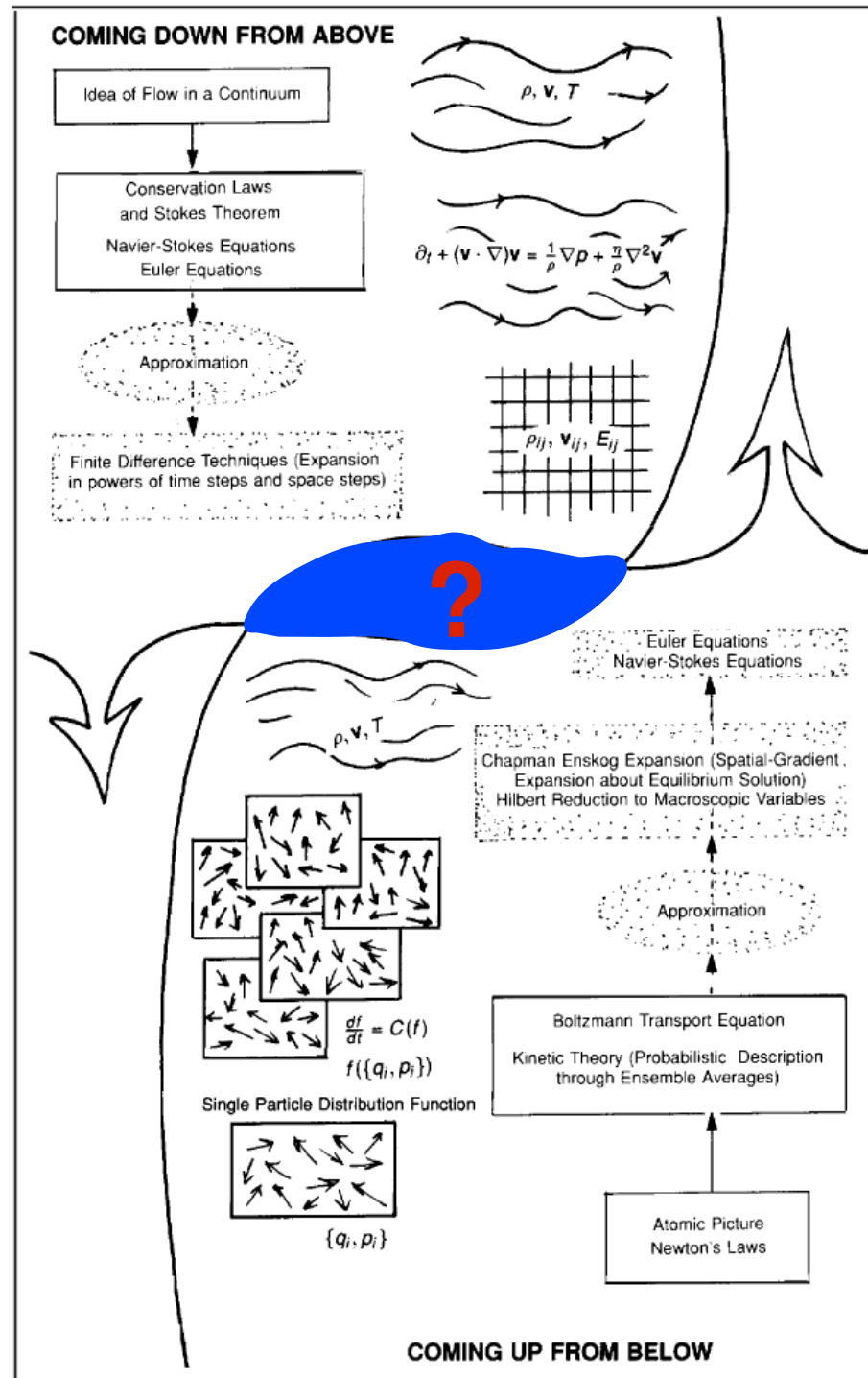
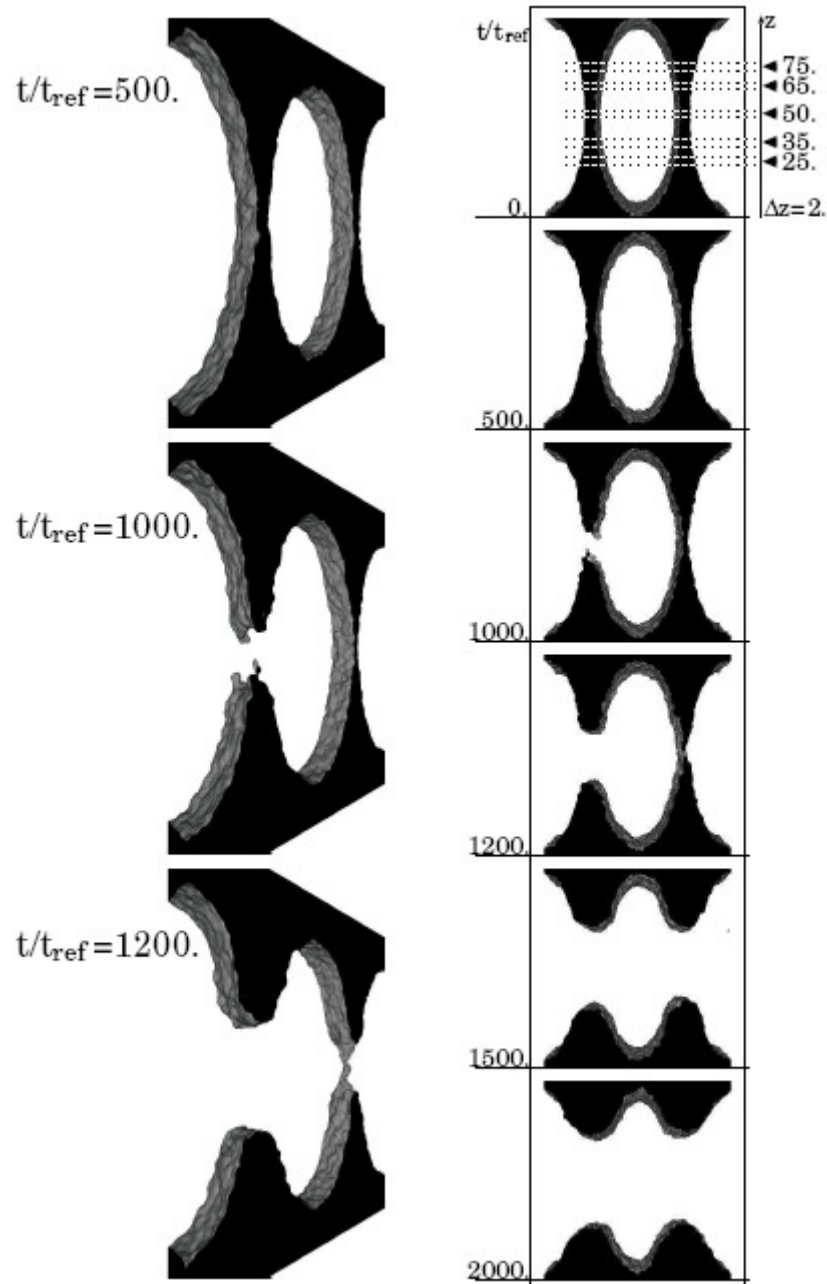
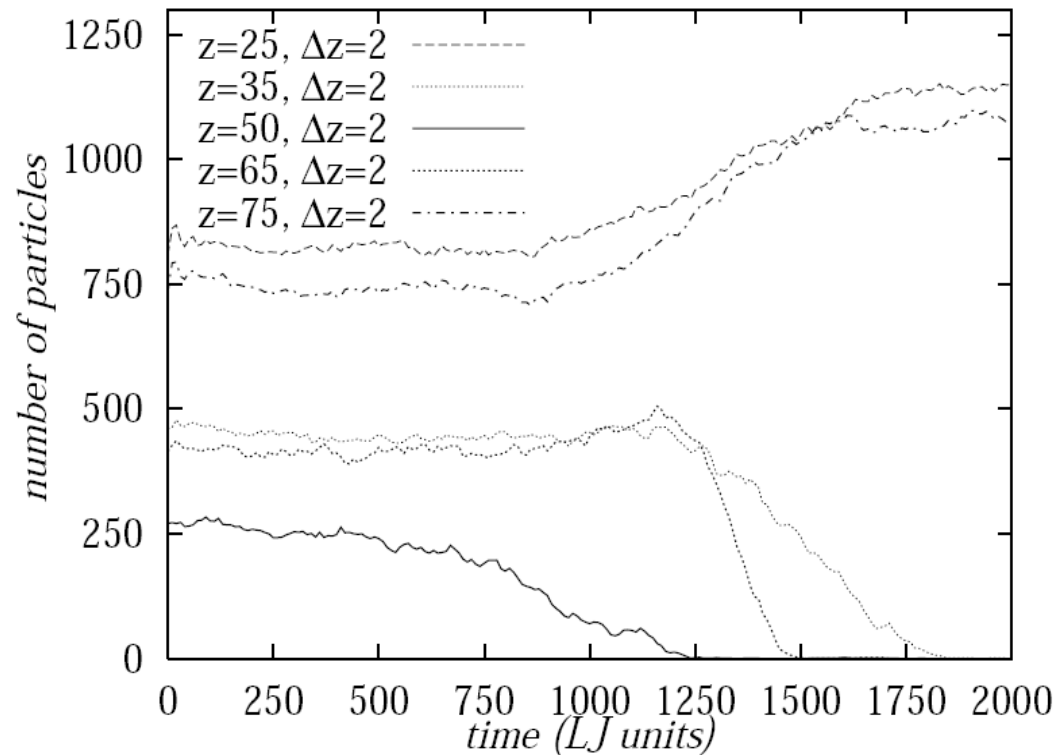


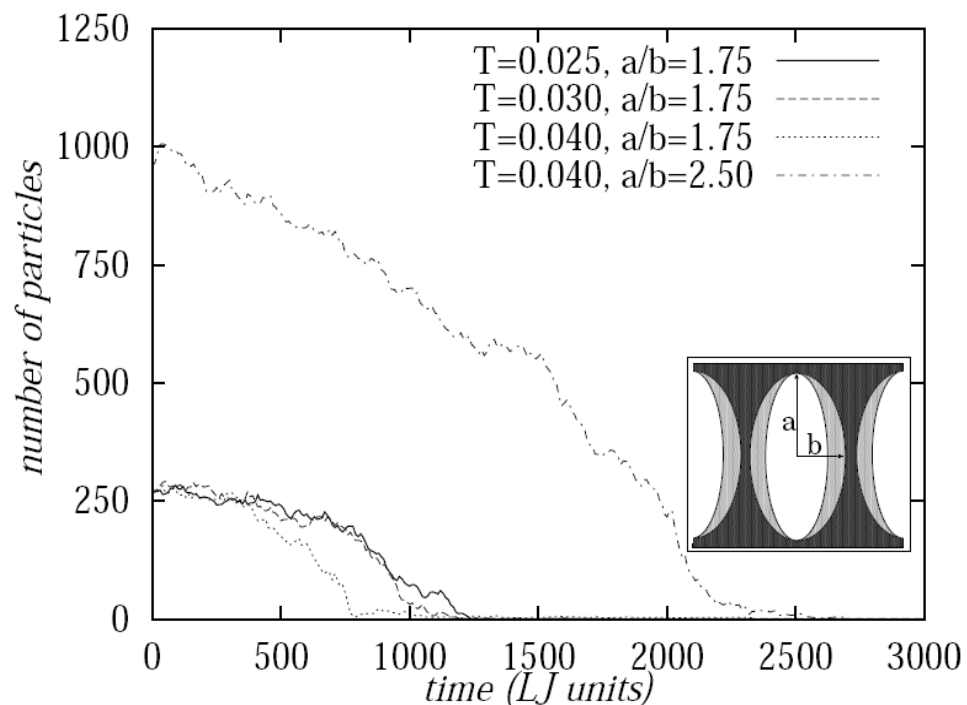
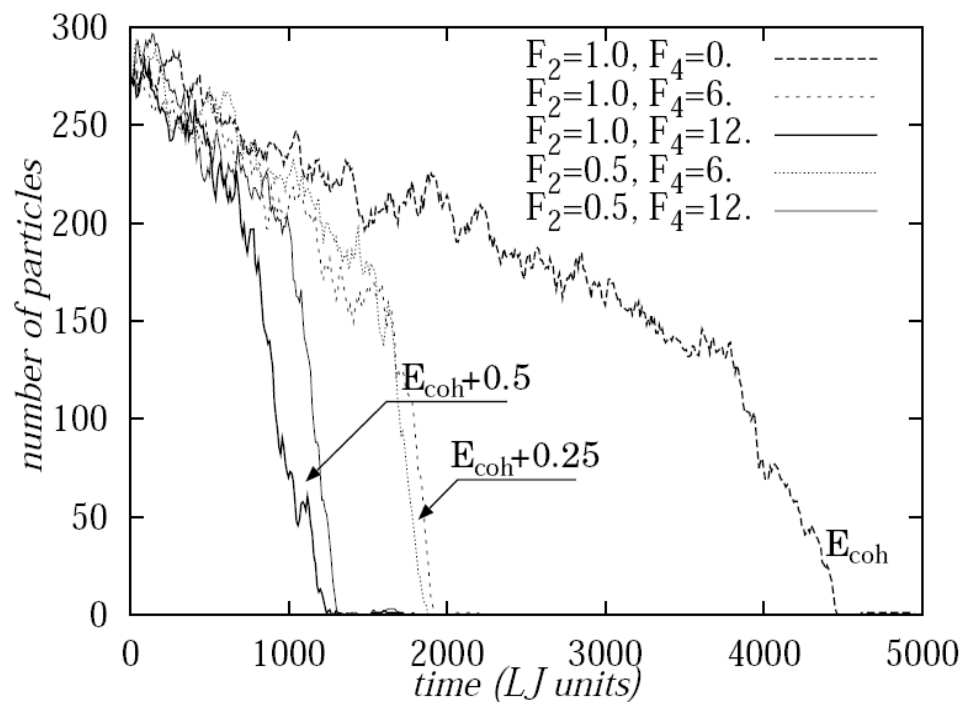
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Kako integrisati dve skale?



Kako integrisati dve skale?



system (atoms)	r_{ref} (nm)	$E_{\text{ref}}, k_B T$	Γ_{ref} (erg/cm ²)	P_{ref}	t_{ref}	
embedded atoms	0.24	3.45eV, 40kK	0.96	40GPa	0.97×10^{-13} s	
	(8)	0.48	27.6eV		1.92	1.9×10^{-13} s
embedded particles	(64)	0.96	0.2keV		3.83	3.9×10^{-13} s
	(500)	1.92	1.8keV		7.67	7.8×10^{-13} s
	(4000)	3.84	14keV		15.3	0.97×10^{-12} s